

# Computational Aspects of the

# Neodeterministic Seismic Hazard Assessment

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# Neo-deterministic approach

- Modelling of ground shaking scenarios
  - Regional scale: on a grid of sites covering the studied area
  - Local scale: along laterally heterogeneous profiles

# Neo-deterministic approach

# Modelling of ground shaking scenarios

- Regional scale: on a grid of sites covering the studied area
- Local scale: along laterally heterogeneous profiles
- Collection of available data
  - Structural properties
  - Historical seismicity
  - Tectonic regime
  - Active seismogenic zones



- Seismic zonation based on the computation of synthetic seismograms on the nodes of a grid that covers the study area
- Average structural properties
- Simple source model (scaled point source)
- Cut-off frequency I Hz
- Maps of peak displacement, velocity and Design Ground Acceleration
- Easy parametric tests
- Modal summation technique





# Scenarios - Event Scale

- Ground-shaking scenario for a single, specific event
- Average structural properties
- Simple or detailed source model
- Cut-off frequency I or I0 Hz
- Maps of peak displacement, velocity and acceleration
- Modal summation technique





# Scenarios - Local Scale

- Synthetic seismograms computed along selected profiles
- Laterally heterogeneous structural models
- Detailed source model
- Cut-off frequency up to 10 Hz
- Maps of ground motion amplification
- Hybrid technique (modal summation + finite difference)









Synthetic seismograms: the Rayleigh waves modal summation (Panza, 1985)

$$u_{x}^{R}(x,z,\omega) = \sum_{m=1}^{\infty} \frac{e^{-i3\pi/4}}{\sqrt{8\pi\omega}} \frac{e^{-ik_{m}x}}{\sqrt{x}} \frac{\left(\chi_{m}^{R}(h_{s},\omega)\right)}{\sqrt{c_{m}v_{m}I_{m}}} \frac{\left(F_{x}(z,\omega)\right)}{\sqrt{v_{m}I_{m}}}$$
$$u_{z}^{R}(x,z,\omega) = \sum_{m=1}^{\infty} \frac{e^{-i\pi/4}}{\sqrt{8\pi\omega}} \frac{e^{-ik_{m}x}}{\sqrt{x}} \frac{\left(\chi_{m}^{R}(h_{s},\omega)\right)}{\sqrt{c_{m}v_{m}I_{m}}} \frac{\left(F_{z}(z,\omega)\right)}{\sqrt{v_{m}I_{m}}}$$
source structure receiver



Structure definition



🔵 Structure definition <



structure: svalp



I985: it all started...

🔵 Structure definition . 🙂



Structure definition



Structure definition 😬

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LIQUID PART THICKNESS THKSEA(I) 0.00000E+00 SOLID PART THICKNESS THKNES(I) 0.20000E+00 0.20000E+00 0.20000E+00 0.20000E+00 0.20000E+00 0.20000E+00 0.20000E+00 0.20000E+00 0.20000E+00 0.20000E+00 0.20000E+00 0.20000E+00 0.20000E+00 0.20000E+00 0.25000E+00 0.25000E+00	DENSITY RHOSEA(I) 0.00000E+00 DENSITY DENSITY RH0(I) 0.28000E+01 0.28000E+01 0.28000E+01 0.28000E+01 0.28000E+01 0.28000E+01 0.28000E+01 0.28000E+01 0.28000E+01 0.28000E+01 0.28000E+01 0.28000E+01 0.28300E+01 0.28300E+01 0.28300E+01 0.28300E+01	P-WAVE VELOCITY ALPSEA(I) 0.00000E+00 	P-WAVE ATTENUATION A2(I) 0.26042E-03 0.26042E-03 0.26042E-03 0.26042E-03 0.26042E-03 0.26042E-03 0.26042E-03 0.26042E-03 0.26042E-03 0.26042E-03 0.26042E-03 0.26042E-03 0.26042E-03 0.21552E-03 0.21552E-03 0.21552E-03	S-WAVE VELOCITY B1(I) 0.24000E+01 0.24000E+01 0.24000E+01 0.24000E+01 0.24000E+01 0.24001E+01 0.24001E+01 0.24001E+01 0.24001E+01 0.24001E+01 0.24002E+01 0.33000E+01 0.33000E+01	S-WAVE ATTENUATI B2(I) 0.10417E- 0.10417E- 0.10417E- 0.10417E- 0.10417E- 0.10417E- 0.10417E- 0.10417E- 0.10417E- 0.10417E- 0.10417E- 0.10417E- 0.10417E- 0.10417E- 0.10417E- 0.10417E- 0.10417E- 0.105758E- 0.75758E- 0.75758E-		
LIQUID PART THICKNESS THKSEA(I) 0.00000E+00 SOLID PART THICKNESS THKNES(I) 0.20000E+00 0.20000E+00 0.20000E+00 0.20000E+00 0.20000E+00 0.20000E+00 0.20000E+00 0.20000E+00 0.20000E+00 0.20000E+00 0.20000E+00 0.25000E+00 0.25000E+00 0.25000E+00 0.25000E+00 0.25000E+00	DENSITY RHOSEA(I) 0.00000E+00 DENSITY DENSITY RH0(I) 0.28000E+01 0.28000E+01 0.28000E+01 0.28000E+01 0.28000E+01 0.28000E+01 0.28000E+01 0.28000E+01 0.28000E+01 0.28000E+01 0.28000E+01 0.28000E+01 0.28300E+01 0.28300E+01 0.28300E+01 0.28300E+01 0.28300E+01	P-WAVE VELOCITY ALPSEA(I) 0.00000E+00 	P-WAVE ATTENUATION A2(I) 0.26042E-03 0.26042E-03 0.26042E-03 0.26042E-03 0.26042E-03 0.26042E-03 0.26042E-03 0.26042E-03 0.26042E-03 0.26042E-03 0.26042E-03 0.26042E-03 0.26042E-03 0.21552E-03 0.21552E-03 0.21552E-03	S-WAVE VELOCITY B1(I) 0.24000E+01 0.24000E+01 0.24000E+01 0.24000E+01 0.24000E+01 0.24001E+01 0.24001E+01 0.24001E+01 0.24001E+01 0.24001E+01 0.24002E+01 0.33000E+01 0.33000E+01 0.33000E+01	S-WAVE ATTENUATI B2(I) 0.10417E- 0.10417E- 0.10417E- 0.10417E- 0.10417E- 0.10417E- 0.10417E- 0.10417E- 0.10417E- 0.10417E- 0.10417E- 0.10417E- 0.10417E- 0.10417E- 0.10417E- 0.10417E- 0.10417E- 0.105758E- 0.75758E- 0.75758E- 0.75758E-		



Job submission on the Mainframe Computer of the Trieste University:



Job submission on the Mainframe Computer of the Trieste University:



Submit in the evening...



Job submission on the Mainframe Computer of the Trieste University:



Submit in the evening...





- I 985: it all started...
  - Job submission on the Mainframe Computer of the Trieste University:
    - Submit in the evening...
    - Cross fingers...
    - ...
- Get the results in the morning...





- I 985: it all started...
  - Job submission on the Mainframe Computer of the Trieste University:
    - Submit in the evening...
    - Cross fingers...
    - Get the results in the morning...
    - 😬 Maybe...





- I 985: it all started...
  - Job submission on the Mainframe Computer of the Trieste University:
    - Submit in the evening...
      - Cross fingers...
  - ...
- Get the results in the morning...

	Maybe
--	-------

首 Do it again..

	INPUT FOR RAYLEIGH W	AVE	S MODE	S – PART1
	*****	*****	*****	****
	NAME OF STRUCTURE	:	SVALP.S	NAMESTR
	MAXIMUM FREQUENCY	: ÷	0.10000E+02	XMAXFR
n	TOTAL NUMBER OF SOLID LAYERS	:	89	N
	NUMBER OF OCEANIC LAYERS		0	MSMAX
	MAX. NUMBER OF MODES TO BE COMPUTED		0	MODETR
	MANTLE CHANNEL (XMAXFR=10	0===>L	ITHOSPHERIC)	PARAMETERS
	PRESENCE OF TYPE 2 CHANNEL IN LID	:	0	TCHLTD
	S-WAVE VELOCITY OF TYPE2 CHANNEL ( - 129	*):	0.00000E+00	UMIN
	CORRESPONDING S-WAVE PHASE ATTENUATION		0.00000E+00	UMINAT
	S-WAVE VELOCITY AT BOTTOM OF TYPE2 CHAN	NEL :	0.00000E+00	UMAX
	CORRESPONDING S-WAVE PHASE ATTENUATION		0.00000E+00	LIMAXAT
	HIGHEST INTERFACE OF TYPE 1 CHANNEL		27	TTOPMC
	LOWEST INTERFACE OF TYPE 1 CHANNEL		44	TCH1
	MTN S-WAVE VELOCITY IN TYPE 1 CHANNEL		0.33001F+01	BCH
	CORRESPONDING S-WAVE PHASE ATTENUATION		0.75755E-03	BCQQAT
	MAX S-WAVE VELOC (AVER ABOV TYPE1 CHANNI	EL )	0 28501F+01	BLCBST
	MAX S-WAVE PHASE ATT (ABOVE TYPE1 CHANNI	EL) .	0.10/17F_02	BCCBAT
	HAATS WAVE FIRST ATTA (ADOVE FIFTET CHANNI	/ -	0.1041/6-02	DUCINAT



Synthetic seismograms: the Rayleigh waves modal summation (Panza, 1985)





- I991:SH waves as well...
  - Complete synthetic seismograms for multimode for high-frequency multimode SH-waves (Florsch et al., 1991)



- I991:SH waves as well...
  - Complete synthetic seismograms for multimode for high-frequency multimode SH-waves (Florsch et al., 1991)

$$u_{y}^{L}(x,z,\omega) = \sum_{m=1}^{\infty} \frac{e^{-i3\pi/4}}{\sqrt{8\pi\omega}} \frac{e^{-ik_{m}x}}{\sqrt{x}} \frac{\left(\chi_{m}^{L}(h_{s},\omega)\right)}{\sqrt{c_{m}v_{m}I_{m}}} \frac{\left(F_{y}(z,\omega)\right)}{\sqrt{v_{m}I_{m}}}$$
$$u_{x}^{R}(x,z,\omega) = \sum_{m=1}^{\infty} \frac{e^{-i3\pi/4}}{\sqrt{8\pi\omega}} \frac{e^{-ik_{m}x}}{\sqrt{x}} \frac{\left(\chi_{m}^{R}(h_{s},\omega)\right)}{\sqrt{c_{m}v_{m}I_{m}}} \frac{\left(F_{x}(z,\omega)\right)}{\sqrt{v_{m}I_{m}}}$$
$$u_{z}^{R}(x,z,\omega) = \sum_{m=1}^{\infty} \frac{e^{-i\pi/4}}{\sqrt{8\pi\omega}} \frac{e^{-ik_{m}x}}{\sqrt{x}} \frac{\left(\chi_{m}^{R}(h_{s},\omega)\right)}{\sqrt{c_{m}v_{m}I_{m}}} \frac{\left(F_{z}(z,\omega)\right)}{\sqrt{v_{m}I_{m}}}$$
source structure receiver



I991: SH waves as well...

U Structure definition

structure: svalp





- I991: SH waves as well...
  - Job submission on the IBM 3090 Mainframe Computer in Bologna (ENEA):
    - Submit at any time...
    - Cross fingers...
  - ....
    - Get the results in a couple of hours...





- I991:SH waves as well...
  - Complete synthetic seismograms for multimode for high-frequency multimode SH-waves (Florsch et al., 1991)





# I993: Seismic zonation at national scale!

Zoning of the Italian territory in terms of expected peak ground acceleration derived from complete synthetic seismograms (Costa et al., 1993)



## I993: Seismic zonation at national scale!

Zoning of the Italian territory in terms of expected peak ground acceleration derived from complete synthetic seismograms (Costa et al., 1993)





- I993: Seismic zonation at national scale!
  - Job submission on local Unix workstation:
  - <u>•</u>
    - Submit at any time...
    - Get the results in a day...





I 993: Seismic zonation at local scale!



## I993: Seismic zonation at local scale!

A new method for the realistic estimation of seismic ground motion in megacities: the case of Rome (F\u00e4h et al, 1993)





## I993: Seismic zonation at local scale!

Job submission on local Unix workstation:



### Submit any time...



#### Get the results in a week...





### I993: Seismic zonation at local scale!

A week, that is, about the same time that it took to prepare a model...

model t1.			dx=dz	=0.005 km	depth= 24	4 <b>.0</b> 25km		
ibsta	rt ibsto	p iclay	/ iclayl	iclayr	nout ndis	nvel nac	c ngsp nb	wd
	1	2 2	2 1	0	4 1	1	1 1	1
1	t0	tstep	)	s0	sstep	ti	me0	
3.000	00	2.00000	0 0	.51000	0.02000	3.0	0000	
fre	eq	d>	C	dz md	im ndim nlr	nax ms	ns nfb	nf
10.000	00	0.00500	0 0	.00500 5	04 522	6 102	0 46	10
thkne	es	rł	1 I	a1	dqa		b1	dqb
2.000	00	2.80000	) 4	.80000	400.00000	2.4	0000 2	00.00000
2.000	00	2.83000	) 5	.80000	400.00000	3.3	0000 2	00.00000
2.000	00	2.84000	6 6	.20000	400.00000	3.5	0000 2	00.00000
8.000	00	2.85000	) 5	.70000	400.00000	3.3	0010 2	00.00000
2.000	00	2.86000	6 6	.20000	400.00000	3.5	5000 2	00.00000
21.050	00	2.87000	6 (	.50000	400.00000	3.7	0000 2	00.00000
dma	dmx	dna	dnz	drho	da1	dqa	db1	dqb
0.0000 0	.4975 0	.0000	2.0000	2.800	4.800	397.100	2.400	180.500 1
0.0000 0	.4975 2	.0000	4.0000	2.830	5.800	397.100	3.300	180.500 1
0.0000 0	.4975 4	.0000	6.0000	2.840	6.200	397.100	3.500	180.500 1
0.0000 0	.4975 6	.0000 1	L4.0000	2.850	5.700	397.100	3.300	180.500 1
0.0000 0	.4975 14	.0000 1	16.0000	2.860	6.200	397.100	3.550	180.500 1
0.0000 0	.4975 16	.0000 3	37.0500	2.870	6.500	397.100	3.700	180.500 1
0.0000 0	.4475 0	.0000	2.0000	2.800	4.800	354.200	2.400	161.000 1
0.0000 0	4475 2	.0000	4.0000	2.830	5.800	354.200	3.300	161.000 1
0.0000 0	.44/5 4	.0000	6.0000	2.840	6.200	354.200	3.500	161.000 1
0.0000 0	.44/5 6	.0000	14.0000	2.850	5.700	354.200	3.300	161.000 1
0.0000 0	.44/5 14	.0000	10.0000	2.800	6.200	354.200	3.550	101.000 1
0.0000 0	.44/5 10	.0000 :	37.0500	2.8/0	0.500	354.200	3.700	161.000 1
0.0000 0	.39/5 0 2075 2	.0000	2.0000	2.800	4.800	311.300	2.400	141.500 1
0.0000 0	-39/5 Z	.0000	4.0000	2.830	5.000	311.300	3.300	141.500 1
0.0000 0	2075 6	.0000	0.0000	2.040	5 700	211 200	2 200	141.500 1
0.0000 0	2075 14	.0000 1	16 0000	2.000	6 200	311.300	3.500	141.500 1
0.0000 0	3075 16	0000	27 0500	2.800	6 500	311 300	3 700	141.500 1
0.0000 0	3475 0	0000	2 0000	2 800	1 800	268 400	2 400	122 000 1
0.0000 0	3475 2	.0000	4.0000	2.830	5.800	268,400	3,300	122.000 1
0.0000 0	3475 4	.0000	6.0000	2.840	6.200	268,400	3.500	122.000 1
0.0000 0	.3475 6	.0000 1	4.0000	2.850	5.700	268,400	3,300	122.000 1
0.0000 0	.3475 14	.0000 1	6.0000	2.860	6.200	268,400	3,550	122.000 1
0.0000 0	.3475 16	.0000 3	37.0500	2.870	6.500	268.400	3.700	122.000 1
0.0000 0	.2975 0	.0000	2.0000	2.800	4.800	225.500	2.400	102.500 1
0.0000 0	2975 2	.0000	4.0000	2.830	5.800	225.500	3.300	102.500 1
0.0000 0	.2975 4	.0000	6.0000	2.840	6.200	225.500	3.500	102.500 1
0.0000 0	.2975 6	.0000 1	14.0000	2.850	5.700	225.500	3.300	102.500 1
0.0000 0	2975 14	.0000 1	16.0000	2.860	6.200	225.500	3.550	102.500 1
0.0000 0	.2975 16	.0000 3	37.0500	2.870	6.500	225.500	3.700	102.500 1
0.0000 0	.2475 0	.0000	2.0000	2.800	4.800	182.600	2.400	83.000 1
0.0000 0	.2475 2	.0000	4.0000	2.830	5.800	182.600	3.300	83.000 1
0.0000 0	.2475 4	.0000	6.0000	2.840	6.200	182.600	3.500	83.000 1
0.0000 0	.2475 6	.0000 1	L4.0000	2.850	5.700	182.600	3.300	83.000 1
0.0000 0	.2475 14	.0000 1	L6.0000	2.860	6.200	182.600	3.550	83.000 1
0.0000 0	.2475 16	.0000 3	37.0500	2.870	6.500	182.600	3.700	83.000 1



## Seismic zonation at national scale

Executing the same computation on modern desktop or laptop computers is a matter of hours...



### Seismic zonation at local scale

- Executing the same computation on modern desktop or laptop computers is a matter of hours...
- ... and preparing the model is even faster than that








Regional polygons					
I-D layered anelastic structures					
Structural model					



Regional polygons						
I-D layered anelastic structures						
Structural model						







Regional polygons
I-D layered anelastic structures
Structural model

Polygons the region0001	at define	e different	structural	regions	(lon,lat)
<b>j</b>	12,550	38.070			
	12.770	38,200			
	12,940	38,050			
	13.090	38.090			
	13.070	38.160			
	13.350	38.250			
	13,450	38,125			
	13.550	38,135			
	13.800	37.980			
	14.025	38.050			
	14.650	38.070			
	14.780	38,180			
	14,980	38.200			
	15,110	38,150			
	15.300	37.810			
	15,140	37.370			
	14,280	37.070			
	13,940	37.080			
	12,980	37,580			
	12.690	37.549			
	12.460	37.800			
region0002	121100	571000			
regionovoz	15,110	38,150			
	15.300	37.810			
	15,680	38,235			
	15,690	37,950			
	16,100	37.900			
	101100	571500			
	15,140	37.370			
	15.323	37.264			
	15.381	37.030			
	15,160	36.795			
	15,190	36.641			
	14.501	36.801			
	14.280	37.070			
region0016					
	13,900	45.550			
	13,680	45.550			
	13,680	45.650			
region0252	10.000				
	13,850	45,900			
	13,950	45.638			
	13.900	45.550			
	13.500	45.750			
	13.500	45.900			
	101000				



Regional polygons					
I-D layered anelastic structures					
Structural model					





		thk(km)	rho	Vp(km/s)	Vs(km/s)	Qp	Qs	depth(km)	layer	
		0.5000	2.300	3.800000	2.200000	660.00	300.00	0.50000	1	
		0.5000	2.300	3.900000	2.250000	660.00	300.00	1.00000	2	
		1.0000	2.450	4.000000	2.300000	660.00	300.00	2.00000	3	
		4.0000	2.450	4.800000	2.700000	660.00	300.00	6.00000	4	
1		3.0000	2.600	5.900000	3.350000	660.00	300.00	9.00000	5	
		5.0000	2.700	6.500000	3.700000	660.00	300.00	14.00000	6	
6.0000	6.0000		2.800	7.000000	4.000000	660.00	300.00	20.00000	7	
8.0000 2.80	8.0000 2.80	2.80	0	6.700000	3.750200	660.00	300.00	28.00000	8	
3.0000 2.85	3.0000 2.85	2.85	0	6.700000	3.750300	660.00	300.00	31.00000	9	
1.0000 2.90	1.0000 2.90	2.90	0	7.000000	4.000000	660.00	300.00	32.00000	10	
68.0000 3.350	68.0000 3.350	3.350		8.000000	4.500000	660.00	300.00	100.00000	11	
100.0000 3.400 8	100.0000 3.400 8	3.400 8	8	.000000	4.150600	220.00	100.00	200.00000	12	
10.0000 3.450	10.0000 3.450	3.450		8.200000	4.400000	220.00	100.00	210.00000	13	
10.0000 3.450	10.0000 3.450	3.450	٥	8.250000	4.450000	220.00	100.00	220.00000	14	
10.0000 3.450	10.0000 3.450	3.450		8.300000	4.500000	220.00	100.00	230.00000	15	
10.0000 3.450	10.0000 3.450	3.450		8.350000	4.550000	220.00	100.00	240.00000	16	
10.0000 3.450	10.0000 3.450	3.450		8.400000	4.600000	220.00	100.00	250.00000	17	
60.0000 3.500	60.0000 3.500	3.500	ł	8.400000	4.600100	220.00	100.00	310.00000	18	
9.0000 3.50	9.0000 3.50	3.50	00	8.700000	4.750000	330.00	150.00	319.00000	19	
10.0000 3.52	10.0000 3.52	3.52	20	8.740000	4.750100	330.00	150.00	329.00000	20	
	7	25.0000	3.950	9.576000	5.285000	330.00	150.00	565.00000	30	
25.0000 4.	25.0000 4.	4.	000	9.630000	5.313000	330.00	150.00	590.00000	31	
25.0000 4	25.0000 4		1.050	9.683000	5.340000	330.00	150.00	615.00000	32	
25.000	25.000	0	4.100	9.736000	5.367000	374.00	170.00	640.00000	33	
		25.0000	4.200	9.782000	5.390000	440.00	200.00	665.00000	34	
25.0	25.0	000	4.250	10.014000	5.518000	506.00	230.00	690.00000	35	
		25.0000	4.300	10.180000	5.630000	572.00	260.00	715.00000	36	
25.0	25.0	000	4.350	10.190000	5.746000	638.00	290.00	740.00000	37	
25.000	25.000	0	4.400	10.492000	5.850000	704.00	320.00	765.00000	38	
		25.0000	4.410	10.677000	5.950000	770.00	350.00	790.00000	39	
25.00	25.00	000	4.420	10.852000	6.044000	836.00	380.00	815.00000	40	
25.	25.	0000	4.425	11.025000	6.140000	902.00	410.00	840.00000	41	
25.0	25.0	000	4.435	11.180000	6.230000	968.00	440.00	865.00000	42	
		25.0000	4.450	11.224000	6.250000	1045.00	475.00	890.00000	43	I
		25.0000	4.475	11.267000	6.275000	1100.00	500.00	915.00000	44	L
		25.0000	4.500	11.310000	6.297000	1166.00	530.00	940.00000	45	I
25.0000	25.0000	24	4.525	11.350000	6.322000	1232.00	560.00	965.00000	46	
25.0000 4.5	25.0000 4.5	4.5	50	11.392000	6.340000	1320.00	600.00	990.00000	47	
25.0000 4.5	25.0000 4.5	4.5	575	11.434000	6.360000	1375.00	625.00	1015.00000	48	
25.0000	25.0000	4	4.600	11.476000	6.375000	1452.00	660.00	1040.00000	49	
25.00	25.00	000	4.630	11.518000	6.390000	1507.00	685.00	1065.00000	50	
25,0000	25 0000		4 660	11 560000	6 405000	1584 00	720 00	1000 00000	51	
-	<b>4</b>	2.0000	000	11.200000	01403000	1304.00	/20100	1030.00000	21	
		25.0000	4.680	11.600000	6.421000	1650.00	750.00	1115.00000	52	











Earthquake Seismogenic zones Focal mechanisms



Earthquake

catalogue





### Regional scale - Sources

Earthquake catalogue

Seismogenic Focal mechanisms

zones

1005	00	0	0	0	4347	1188	0520520	05200
1005	00	0	0	0	4150	1375	0520520	05200
1065	327	11	0	0	4553	1022	0520520	05200
1087	90	0	0	0	4125	1560	0500500	05000
1097	00	0	0	0	4560	1530	0620620	06200
1117	13	13	0	0	4545	1104	0640640	06400
1120	00	0	0	0	4142	1387	0550550	05500
11251	011	0	0	0	4113	1478	0550550	05500
1139	122	0	0	0	4110	1483	0420420	04200
1148	00	0	0	0	4377	1123	0500500	05000
1168	110	0	0	0	4372	1040	0420420	04200
1169	24	0	0	0	3733	1520	0730730	07300
1170	39	0	0	0	4157	1333	0520520	05200
1182	815	0	0	0	4442	890	0440440	04400
1988	315	12	3	0	4483	1073	5440360	04400
1988	426	05	53	0	4228	1658	5450450	0 00
19881	028	184	48	0	3780	1509	5350320	03500
1989	913	215	54	0	4587	1118	10470400	04700
19891	023	211	19	0	4175	1273	5440350	04400
19891	226	195	59	0	4352	755	5440440	0 00
1990	55	72	21	0	4073	1563	10500390	05000
19901	213	02	24	0	3727	1507	5530530	05200
1991	526	122	26	0	4069	1574	5470390	04700
19911	120	15	54	0	4674	946	5520520	0 00
1992	218	33	30	0	4226	1418	5420360	04200



Earthquake catalogue Seismogenic rocal mechanisms







Earthquake catalogue Seismogenic zones Focal mechanisms

Polygons th	at define	e seismogenic	zones	(lon,lat)
seismo0257				
	15.278	44.918		
	15.036	44.635		
	14.644	44.783		
	14.422	45.193		
	14.890	45.500		
seismo0004				
	12.520	46.468		
	13.300	46.550		
	13.600	46.450		
	13.580	46.400		
	13.160	46.156		
	12.636	45.972		
	12.403	45.840		
seismo0079				
	14.955	37.582		
	15.196	37.529		
	15.273	37.511		
	15.486	36.630		
	14.984	36.582		
	14.969	37.098		
seismo0081				
	19.334	39.834		
	19.110	39.310		
	18,618	39,527		
	18,911	40.190		



Earthquake catalogue Seismogenic zones Focal mechanisms







Earthquake Seismogenic Focal mechanisms

44A 19591223 929000 37.720N 14.610E 770 0 0 0 053 SICILY 00044F 077 43 004 344 87 132 041 29 289 34 161 43 0001 SICILY 54A 19671031 2108000 37.840N 14.600E 380 0 0 0 050 SICILY 00054F 009 61 189 274 80 333 228 27 324 13 077 60 0001 SICILY 57A 19680115 133000 37.890N 13.080E 200 0 0 0 051 SICILY 00057F 040 82 046 302 46 168 163 23 272 37 049 45 0001 SICILY 58A 19680115 201000 37.780N 13.030E 30 0 0 0 054 SICILY 00058F 204 70 015 108 75 159 157 04 065 25 255 65 0001 SICILY

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#### Sources



Magnitude discretization and smoothing



#### Sources

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Why do we do this?



Magnitude discretization and smoothing





#### Sources

Why do we do this?

To account for mislocations of events in the catalogue



Magnitude discretization and smoothing



Why do we do this?

To account for mislocations of events in the catalogue

To account (roughly) for fault dimensions



#### Sources



Magnitude discretization and smoothing





#### Sources

### Why do we do this?

- To account for mislocations of events in the catalogue
- To account (roughly) for fault dimensions
- To account for the location of future events



Magnitude discretization and smoothing





#### Sources

### Why do we do this?

- To account for mislocations of events in the catalogue
- To account (roughly) for fault dimensions
- To account for the location of future events
- In essence: to be conservative...

## Regional scale - Discretized Magnitude



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### Regional scale - Smoothed magnitude



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# Source definition - Radiation pattern


## Source definition - Scaled point source

- The moment-magnitude relation by Kanamori (1977) is used
- At first synthetic seismograms are computed for a unitary scalar seismic moment (I dyn cm)
- Then they are scaled for magnitude in the frequency domain according to the spectral law by Gusev (1983) as reported in Aki (1987)



# Source definition - Scaled point source

### Source kinematic model



2-dimensional final slip distribution over a source rectangle, shown as a density plot (Mw=7.0).

Rupture front evolution was simulated kinematically from random rupture velocity field.

(Gusev, 2011)

Far-field source time histories and their spectra.

"Displacement" far-field functions (arbitrary scale) for the simulated case of mostly unilateral rupture propagation



## Example computation - Ground shaking



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# Example computation - Ground shaking



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## Example computation - Ground shaking



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## From IHz acceleration to DGA

To obtain an estimate of PGA, overcoming the I Hz limitation chosen in the modelling, the shape of Design Spectra can be used







# From IHz acceleration to DGA

The procedure gives good results when applied to the case of the Irpinia 1980 earthquake. The DGA predicted by the modelling is similar the actual DGA obtained from recordings



# Regional Scale - Check (I Hz cutoff)

Friuli, 6 May 1976 (North-Eastern Italy)

Irpinia, 23 October 1980 (Southern Italy)



# Regional Scale - Check (I Hz cutoff)



Irpinia, 23 October 1980 (Southern Italy)

process is not known a priori



### Parametric Test on Earthquake Catalogue



**CPTI - UCI** 





### Parametric Test on Earthquake Catalogue



A (g)

0.209

0.150

0.080

0.040

0.020

0.010

CPTI - UCI



### Regional Scale - Homogeneity!

If seismogenic zones are not defined according to homogeneous criteria, hazard results will be hardly comparable (source: GSHAP)



Fig. 2. Final distribution of earthquake source zones for the Ibero-Maghreb region, and epicenters of the generated List of Significant Earthquakes with  $M \ge 4.5$  from 1900 to 1989.

# Regional Scale - Homogeneity!



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# Regional Scale - Implementation







### Local Scale - Definition of Model

### Modal Summation

Finite Difference





### Local Scale - Definition of Model

### Modal Summation

Finite Difference





### Local Scale - Definition of Model

### Modal Summation





Parameters file for program pfdq10 \_\_\_\_\_ Modal summation model Modes for 1D structure test.spr 0 First mode to use (1=fundamental, 0=all) 0 Last mode to use (0=all) Low pass filter cutoff frequency (xcutof) 10.0 Ratio between filter's max freq with unit response and xcutof .50 .02 Low pass filter amplitude at cutoff Interpolation for modal summation part 0 5.000 Source depth (km) 125.0 strike-receiver angle (SH modelling) 45.0 fault dip (SH modelling) 90.0 fault rake (SH modelling) 125.0 strike-receiver angle (P-SV modelling) 45.0 fault dip (P-SV modelling) 90.0 fault rake (P-SV modelling) 7.5 Source-2D model origin distance (km) \_\_\_\_\_ Finite differences model \_\_\_\_\_ Generated FD model test Polygons with 2D part definition test.pof 2800 Max number of grid points along x 600 Max number of grind points along z 0 Force an air layer of 5 grid points without topography (0=no, 1=yes) Min velocity (km/s) for grid definition (0=auto -> look for min Vs) 0.0 0 FD model length from 1st column of seismograms (km) (0=auto) FD model depth (km) (0=auto) 0.00 0.000 Grid spacing (km) (0=auto) 0 dz multiplier (0=auto) Depth where step along z changes (0=auto) 0.000 Number of absorbing points along x (0=auto) 0 Number of absorbing zones (0=auto) 0 0 Lowest Q for absorbing zones (0=auto) Highest Q for absorbing zones (0=auto) 0 1 Geom. spreading (0=no, 1=yes) for SH (suggested: 0 far/short,1 near/long) Geom. spreading (0=no, 1=yes) for P-SV (suggested: 1) 1 10 Time window length (s) for 1D SH (0=auto) 10 Time window length (s) for 1D P-SV (0=auto) Time window length (s) for 2D SH (0=auto) 10

- 10 Time window length (s) for 2D P-SV (0=auto)
- 00 Shift in origin time (SH)
- 00 Shift in origin time (P-SV)

#### Modal Summation

### Finite Difference





FORTRAN codes

gfortran compiler (any should work)













## Local Scale - Choice of Scenario Earthquakes

- Regional zonation
- Morphostructural analysis
- Active faults
- Earthquake prone areas











### Profiles definition in Google Earth





### Local Scale - Choice of Profiles

### Definition of the profile topography





### Drawing of the profile with XDigiMac



### Local Scale - Choice of Profiles

### Main elements of XDigiMac user interface





### Local Scale - Preliminary Parametric Test

- Radiation Pattern
  - Source Depth
  - Epicentral Distance
  - 8 ....





### Local Scale - Synthetic Seismograms 2D



Depth (km)

#### Radial Acceleration

0.0100394

30

Time (s)

35

40

45

#### Radial Velocity

#### Radial Displacement

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10	1 1 5 20	25	30	1	1	45	

4.72851e-05

Time (s)

Time (s)

30

35

40

45

25

20





Intern

# 0

### Local Scale - Seismograms and Response

### Same site at the intersection of two profiles (red triangle)





### Seismic Source of finite dimension and complicated rupturing process



### Local Scale - Differential Motion

### Significant for elongated structures (bridges, lifelines etc)



# Local Scale - Engineering Analysis

- The data set of synthetic seismograms can be used and analysed by civil engineers for design and reinforcement actions, and therefore supply a particularly powerful and economical tool for the prevention aspects of Civil Defence.
- Evaluate the response of relevant manmade structures, in terms of displacements and stresses, with respect to a set of possible scenario earthquakes











Not fully satisfied with shell scripts



Not fully satisfied with shell scripts

How to reach the potential adopters?


Not fully satisfied with shell scripts

How to reach the potential adopters?

Web application!



Web Application developed in the framework of the Project: Definition of seismic hazard scenarios and microzoning by means of Indo-European e-infrastructures Sponsored by Regione Friuli Venezia Giulia Version 0.16.0 hosted on VacRBook.local, connected from IP 127.0.0.1







User:	Enter
Password:	



See you at the computer exercise session!



000	XeRiS – Login
eRiS	Version 0.9.5.1 hosted on hazard.vm, connected from IP 172.16.10.1
Cuest   Registered User   User:   Password:	

0





00			XeRiS - Sources	Vere 0.0	E 1 on barard un
Structure Eigen Source Parametrie Browse Compute	c Scenario 2D Scenario	Regional Hazard Tsunam	ni Ad	vers. 0.9 1in Help	Logout Admin
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#### Optimization

- Identification of critical package programs
- Identification of hot spots within programs

#### Porting to grid or cloud infrastructure



Data management



## Flow chart of the package - Optimization





2011/04/1513:01:55esgr0050computing74 seismograms for structure n. 1 (index 0010)2011/04/1513:02:14esgr0050radial components computed and rotated to NS and EW2011/04/1513:02:14esgr0050OK - Execution terminated



## Optimization - Seismogram computation

Removed repeated formatted disk I/O, defined new arrays instead

6.5 hours 2 hours (Rayleigh waves) (3.25 x speedup) 5 hours 1.3 hours (Love waves) (3.8 x speedup)

Tested further optimization: sorting seismograms by source depth





#### Flow chart of the package - Grid





#### Project tasks - Grid

- Add to the package a FORTRAN program that perturbs the properties of the earthquake source (orientation and depth, four parameters changed in loops)
- Prepare a shell script to generate as many JDL scripts as the combinations of parameters are, and submits all the combinations to the grid in a single command
- Improve the job submission
- 🔵 Manage data retrieval

#### Further possible optimization...

- Vectorization and parallelization
  - FFT routines
  - modal summation technique

$$u_{y}^{L}(x,z,\omega) = \sum_{m=1}^{\infty} \frac{e^{-i3\pi/4}}{\sqrt{8\pi\omega}} \frac{e^{-ik_{m}x}}{\sqrt{x}} \frac{\left(\chi_{m}^{L}(h_{s},\omega)\right)}{\sqrt{c_{m}v_{m}I_{m}}} \frac{\left(F_{y}(z,\omega)\right)}{\sqrt{v_{m}I_{m}}}$$
$$u_{x}^{R}(x,z,\omega) = \sum_{m=1}^{\infty} \frac{e^{-i3\pi/4}}{\sqrt{8\pi\omega}} \frac{e^{-ik_{m}x}}{\sqrt{x}} \frac{\left(\chi_{m}^{R}(h_{s},\omega)\right)}{\sqrt{c_{m}v_{m}I_{m}}} \frac{\left(F_{x}(z,\omega)\right)}{\sqrt{v_{m}I_{m}}}$$
$$u_{z}^{R}(x,z,\omega) = \sum_{m=1}^{\infty} \frac{e^{-i\pi/4}}{\sqrt{8\pi\omega}} \frac{e^{-ik_{m}x}}{\sqrt{x}} \frac{\left(\chi_{m}^{R}(h_{s},\omega)\right)}{\sqrt{c_{m}v_{m}I_{m}}} \frac{\left(F_{z}(z,\omega)\right)}{\sqrt{v_{m}I_{m}}}$$
source structure receiver



See you at the computer exercise session!

